



higher education & training

Department:
Higher Education and Training
REPUBLIC OF SOUTH AFRICA

NASIENRIGLYN

NASIONALE SERTIFIKAAT STERKTE- EN STRUKTUURLEER N6

12 AUGUSTUS 2019

Hierdie nasienriglyn bestaan uit 8 bladsye.

VRAAG 1

1.1 by 200 mm : $a + \frac{b}{0,2^2} = 30 \times 10^6 \dots \dots \dots \quad (1) \checkmark$

by 140 mm : $a + \frac{b}{0,14^2} = 0 \dots \dots \dots \quad (2) \checkmark$

$$(1) - (2) : 25b - 51,02b = 30 \times 10^6$$

$$b = -1,153 \times 10^6 \checkmark$$

$$a = 58,824 \times 10^6 \checkmark$$

$$\sigma_{Hmin} = a - \frac{b}{0,2^2} = 58,824 \times 10^6 - \frac{(-1,153 \times 10^6)}{0,2^2} \checkmark = 87,647 MPa \checkmark \quad (6)$$

1.2 by 200 mm : $a + \frac{b}{0,2^2} = 30 \times 10^6 \dots \dots \dots \quad (1) \checkmark$

by 250 mm : $a + \frac{b}{0,25^2} = 0 \dots \dots \dots \quad (2) \checkmark$

$$(1) - (2) : 25b - 16b = 30 \times 10^6$$

$$b = 3,333 \times 10^6 \checkmark$$

$$a = -53,333 \times 10^6 \checkmark$$

$$\sigma_{Hmax} = a - \frac{b}{0,2^2} = -53,333 \times 10^6 - \frac{(3,333 \times 10^6)}{0,2^2} \checkmark = -136,667 MPa \checkmark \quad (6)$$

1.3 $\delta d_1 = \frac{D_c}{E} (\sigma_H - \vartheta \times \sigma_R)$

$$= \frac{0,2}{200 \times 10^9} (87,647 \times 10^6 - 0,3 \times 30 \times 10^6)$$

$$\delta d_1 = 78,647 \times 10^{-6} m \checkmark \quad (1)$$

1.4 $\delta d_2 = \frac{D_c}{E} (\sigma_H - \vartheta \times \sigma_R)$

$$= \frac{0,2}{200 \times 10^9} (-136,667 \times 10^6 - 0,3 \times 30 \times 10^6)$$

$$\delta d_2 = -145,667 \times 10^{-6} m \checkmark \quad (1)$$

1.5 $\Delta d = \delta d_1 - \delta d_2$
 $= 78,647 \times 10^{-6} - (-145,667 \times 10^{-6})$
 $\Delta d = 0,224 mm \checkmark$

(1)
[15]

VRAAG 2

2.1 $M = \frac{wL^2}{8} = \frac{12 \times 10^3 \times 4^2}{8} = 24 \text{ kNm } \checkmark$

$$Z = \frac{M}{\sigma} = \frac{24 \times 10^3}{80 \times 10^6} = 300 \times 10^{-6} \text{ m}^3 \checkmark$$

Ligste profiel is 305 × 102 × 28,6 kg/m ✓ (Z = 352,1 × 10⁻⁶m³) (3)

2.2 $y = \frac{5wL^4}{384EI}$

$$\frac{4}{360} \checkmark = \frac{5 \times 12 \times 10^3 \times 4^4}{384 \times 207 \times 10^9 \times I}$$

$$I = 17,391 \times 10^{-6} \text{ m}^4 \checkmark$$

Ligste profiel is 305 × 102 × 24,5 kg/m ✓ (I = 43,64 × 10⁻⁶m⁴) (3)

2.3 *Korrekte profiel is 305 × 102 × 28,6kg/m ✓*

Hierdie profiel sal sowel spanning – as defleksiegrense bevredig ✓ (2)

2.4 $\sigma = \frac{M}{Z} = \frac{24 \times 10^3}{352,1 \times 10^{-6}} = 68,162 \text{ MPa } \checkmark$

$$y = \frac{5wL^4}{384EI} = \frac{5 \times 12 \times 10^3 \times 4^4}{384 \times 207 \times 10^9 \times 43,64 \times 10^{-6}} = 4,428 \text{ mm } \checkmark$$

(2)
[10]

VRAAG 3

$$3.1 \quad A = \frac{\pi(D^2 - d^2)}{4} = \frac{\pi \times (2,8^2 - 2,6^2)}{4} = 0,848 \text{ m}^2 \checkmark$$

$$I = \frac{\pi(D^4 - d^4)}{64} = \frac{\pi(2^4 - 1,9^4)}{64} = 0,774 \text{ m}^4 \checkmark$$

$$W = \rho Ahg = 2400 \times 0,848 \times h \times 9,81 = 19970,728h \checkmark$$

$$F = p \times A_p = 1,2 \times 10^3 \times 2,8 \times h \times 0,6 = 2016h \checkmark$$

$$\sigma_d = \frac{W}{A} = \frac{19970,728h}{0,848} = 23544h \checkmark$$

$$\sigma_b = \frac{FeY}{I} = \frac{2016h \times 0,5h \times 1,4}{0,774} = 1823,233h^2 \checkmark$$

vir geen spanning $\sigma_b = \sigma_d$

$$1823,233h^2 = 23544h \checkmark \\ h = 14,559 \text{ m} \checkmark \quad (8)$$

$$3.2 \quad \sigma_d = 23544h = 23544 \times 14,559 = 342,771 \text{ kPa} = \sigma_b \checkmark$$

$$\sigma_{max} = \sigma_d + \sigma_b = 342,771 + 342,771 = 685,543 \text{ kPa} \checkmark \text{ kompressie} \checkmark \quad (3) \\ [11]$$

VRAAG 4

$$4.1 \quad W_1 = \rho g Al = 2000 \times 9,81 \times 1,2 \times 2,5 \times 1 = 58,86 \text{ kN} \checkmark$$

$$V = W_1 + W_2 = 47,677 + 100 = 158,86 \text{ kN} \checkmark \quad (2)$$

$$4.2 \quad C_\mu = \frac{1 - \sin 30}{1 + \sin 30} = 0,333 \checkmark$$

$$F_g = \frac{\rho gh^2}{2} \times C_\mu = \frac{1680 \times 9,81 \times 2,5^2 \times 0,333}{2} = 17,168 \text{ kN} \checkmark \quad (2)$$

4.3 $W \sim M = W_1 \times x_1 + W_2 \times x_2 = 58,86 \times 0,6 + 100 \times 0,4 = 75,316 \text{ kNm } \checkmark$

$$F \sim M = F_g \times \frac{h}{3} = 17,168 \times 0,833 = 14,306 \text{ kNm } \checkmark$$

$$V \times x + F \sim M = W \sim M$$

$$158,86 \times x + 14,306 = 75,316 \checkmark$$

$$x = 0,384 \text{ m } \checkmark$$

Daar sal spanning wees omdat $x < \frac{B}{3}$ \checkmark (val buite middelste derde) (5)

4.4 $e = 0,5B - x = 0,6 - 0,384 = 0,216 \text{ m } \checkmark$

$$\sigma_{toe} = \frac{V}{B} + \frac{6Ve}{B^2} = \frac{158,86}{1,2} + \frac{6 \times 158,86 \times 0,216}{1,2^2} = 275,326 \text{ kPa (komp)} \checkmark$$

$$\sigma_{heel} = \frac{V}{B} - \frac{6Ve}{B^2} = \frac{158,86}{1,2} - \frac{6 \times 158,86 \times 0,216}{1,2^2} = -10,559 \text{ kPa (trek)} \checkmark \quad (3)$$

4.5 $\sigma_{ult} = \sigma_{max} \times FOS = 275,326 \times 3 \checkmark = 825,978 \text{ kPa } \checkmark \quad (2)$
[14]

VRAAG 5

5.1 $L = \sqrt{\frac{W_T}{p}} = \sqrt{\frac{2,4 \times 10^6 + 300 \times 10^3}{200 \times 10^3}} \checkmark = 3,674 \text{ m } \checkmark$

5.2 $M = \frac{W(L-l)}{8} = \frac{2,4 \times 10^6(3,674 - 0,8)}{8} \checkmark = 862,27 \text{ kNm } \checkmark$

5.3 $Z = \frac{M}{\sigma \times n} = \frac{862,27 \times 10^3}{110 \times 10^6 \times 5} = 1567,764 \times 10^{-6} \text{ m}^3 \checkmark$

Ligste I - balk is $457 \times 191 \times 82 \text{ kg/m } \checkmark$ ($Z = 1612 \times 10^{-6} \text{ m}^3$)

5.4 $l = b \times n + 0,075(n-1) = 0,1913 \times 5 + 0,075 \times 4 \checkmark = 1,2565 \text{ m } \checkmark$

5.5 $M = \frac{W(L-l)}{8} = \frac{2,4 \times 10^6(3,674 - 1,2565)}{8} \checkmark = 725,32 \text{ kNm } \checkmark$

5.6 $Z = \frac{M}{\sigma \times n} = \frac{725,32 \times 10^3}{110 \times 10^6 \times 10} = 659,382 \times 10^{-6} \text{ m}^3 \checkmark$

Ligste I - balk is $356 \times 171 \times 44,8 \text{ kg/m } \checkmark$ ($Z = 686,1 \times 10^{-6} \text{ m}^3$)

(6 x 2) [12]

VRAAG 6

6.1 $m A_s (d - n) = A_1 y_1 + A_2 y_2$

$$15 \times 600 \times 10^{-6} (0,6 - n) \checkmark = 0,5 \times 0,1 (n - 0,05) \checkmark + 0,2 \times 0,5 (n - 0,1)^2 \checkmark$$

$$100n^2 + 39n - 6,9 = 0$$

$$n = 0,132 \text{ m } \checkmark \quad (4)$$

6.2 $\frac{\sigma_s}{\sigma_c} = \frac{m(d - n)}{n}$

$$\frac{120 \times 10^6}{\sigma_c} = \frac{15(0,6 - 0,132)}{0,132} \checkmark$$

$$\sigma_c = 2,26 \text{ MPa } \checkmark$$

$$\sigma_s = 120 \text{ MPa } \checkmark \quad (3)$$

6.3 $\sigma_{c1} = \frac{\sigma_c(n - t)}{n} = \frac{2,26 \times 10^6 (0,132 - 0,1)}{0,132} = 0,55 \text{ MPa } \checkmark$ (1)

6.4 $M_c = 0,5 \sigma_c A_c \frac{2}{3} n - \left[0,5 \sigma_{c1} (b - e)(n - t) \frac{2}{3} (n - t) \right]$
 $= 0,5 \times 2,26 \times 500 \times 132 \times \frac{2}{3} \times 132 - 0,5 \times 0,55 \times 300 \times \frac{2}{3} \times 32^2 \checkmark$
 $= 6576,557 - 56,806 \checkmark$

$$M_c = 6519,752 \text{ Nm } \checkmark \quad (3)$$

6.5 $M_s = \sigma_s A_s (d - n) = 120 \times 10^6 \times 600 \times 10^{-6} (0,6 - 0,132) = 33685,434 \text{ Nm } \checkmark$

$$M = M_c + M_s = 6,5198 + 33,685 = 40,205 \text{ kNm } \checkmark \quad (2)$$

[13]

VRAAG 7

$$7.1 \quad \frac{wx_1^2}{2d} = \frac{w(L - x_1)^2}{2(d + h)}$$

$$\frac{x_1^2}{8} = \frac{(160 - x_1)^2}{14} \quad \checkmark$$

$$\frac{160 - x_1}{x_1} = \sqrt{\frac{14}{8}} \quad \checkmark$$

$$x_1 = 68,88 \text{ m} \quad \checkmark \quad (3)$$

$$7.2 \quad F_H = \frac{wx_1^2}{2d} = \frac{15 \times 10^3 \times 68,88^2}{2 \times 8} \quad \checkmark = 4447,944 \text{ kN} \quad \checkmark \quad (2)$$

$$7.3 \quad F_{v2} = wx_2 = 15 \times 10^3 \times 91,12 = 1366,798 \text{ kN} \quad \checkmark$$

$$F_{T2} = \sqrt{F_H^2 + F_{v2}^2} = \sqrt{4447,944^2 + 1366,798^2} = 4653,208 \text{ kN} \quad \checkmark \quad (2)$$

$$7.4 \quad \text{By } 120 \text{ m vanaf laer steunstuk: } x_3 = 120 - x_1 = 51,12 \text{ m} \quad \checkmark$$

$$F_{v3} = wx_3 = 15 \times 10^3 \times 51,12 = 766,798 \text{ kN} \quad \checkmark$$

$$F_{T3} = \sqrt{F_H^2 + F_{v3}^2} = \sqrt{4447,944^2 + 766,798^2} = 4513,556 \text{ kN} \quad \checkmark \quad (3)$$

[10]

VRAAG 8

$$8.1 \quad R_L \times 1,2 = 2600 \times 0,8 + 981 \times 0,4 + 600 \times 1,2 \times 0,6 \quad \checkmark$$

$$R_L = 2420,333 \text{ N} \quad \checkmark$$

$$R_R \times 1,2 = 2600 \times 0,4 + 981 \times 0,8 + 600 \times 1,2 \times 0,6 \quad \checkmark$$

$$R_R = 1880,667 \text{ N} \quad \checkmark \quad (4)$$

$$8.2 \quad M = 2420,333 \times 0,4 - 600 \times 0,4 \times 0,2 \quad \checkmark = 920,133 \text{ Nm} \quad \checkmark \quad (2)$$

$$8.3 \quad T = (T_1 - T_2)r = (2000 - 600)0,2 = 280 \text{ Nm} \quad \checkmark \quad (1)$$

8.4 $M_e = 0,5 \left(M + \sqrt{M^2 + T^2} \right) = 0,5 \left(920,13 + \sqrt{920,13^2 + 280^2} \right) = 940,963 \text{ Nm } \checkmark$

$$M_e = \frac{\pi d^3 \sigma}{32}$$

$$940,963 = \frac{\pi \times d^3 \times 70 \times 10^6}{32} \checkmark$$

$$d = 51,542 \text{ mm } \checkmark \quad (3)$$

8.5 $M_e = \frac{\pi (D^4 - d^4) \sigma}{32D}$

$$940,963 = \frac{\pi \times [D^4 - (0,5)^4] \times 70 \times 10^6}{32D}$$

$$940,963 = \frac{\pi \times (0,9375D^4)70 \times 10^6}{32D} \checkmark$$

$$\begin{aligned} D &= 52,662 \text{ mm } \checkmark \\ d &= 26,331 \text{ mm } \checkmark \end{aligned} \quad (3)$$

8.6 $\% besparing = \frac{d_s^2 - (D^2 - d^2)}{d_s^2} = \frac{51,542^2 - (52,662^2 - 26,331^2)}{51,542^2} \checkmark$

$$= 21,7\% \checkmark \quad (2)$$

[15]

TOTAAL: 100